Communications

Comments on a Recent Infinitesimal-Deformation Approach to Martensite Crystallography*

HASSEL LEDBETTER and MARTIN DUNN

Recently, Navruz^[1] gave a reformulated infinitesimaldeformation approach to martensite crystallography, and he applied it to the fcc-to-bct transformation in Fe-7Al-2C,^[2,3] That study contained three claims: (1) a better prediction of the shape-deformation magnitude m₁; (2) "excellent" agreement with predictions of the Wechsler-Lieberman-Read/ Bowles-Mackenzie (WLR/BM) invariant-plane-strain theories,^[4,5] and (3) (implied) a simpler alternative to the WLR/ BM theories.

Here, we dispute all of these claims.

The first, and simplest claim is dismissed easily. Navruz claimed that his predicted shape-deformation magnitude $m_1 = 0.1274$ agrees better with observation (0.1220) than the WLR/BM value, 0.1379. However, Watanabe and Wayman^[3] estimated a large error (20.8 pct) in their measured m_1 ; thus, $m_1 = 0.1220 \pm 0.0253$. Their measurement bounds include both the WLR/BM and Navruz predictions.

Second, as for "excellent" agreement between Navruz's theory and WLR/BM, we focus on the habit plane p, which is more sensitive than the orientation relationships discussed by Navruz, Although Navruz calculated p, he failed to point out the 7.3 deg discrepancy between his prediction and the average observed p. This is a large discrepancy. Habit planes are usually measured within 1 deg, and prediction-observation agreement is often within a few degrees. Because Navruz did not report the shape-change direction d, or sufficient information to compute it, we cannot compare his d prediction with the WLR/BM prediction, which would provide another sensitive test. Figure 1 shows the observed, Navruz, and WLR/BM p results plotted in the standard unit triangle. (The WLR/BM p coordinates given by Navruz are incorrect, and about 7 deg from the correct WLR/BM prediction.)

Third, Figure 1 also shows a curious feature of Navruz's **p** prediction: it is confined to the $(0 \ k \ l)$ line, as shown also by the expressions for **p** in his Table II. One lesson from the WLR/BM theories and the related measurements is that habit planes are irrational with general indices $(h \ k \ l)$. The value h = 0 imposes a severe constraint. Thus, the Navruz formulation must fail increasingly as habit planes move away from the $(0 \ k \ l)$ curve. Other formulations of the infinitesimal-deformation approach also encounter the $(0 \ k \ l)$ dilemma, for example, Khachaturyan^[6] and Mura $et \ al.$ ^[7]

Discussion submitted April 9, 2001.

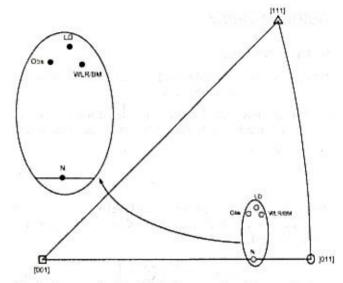


Fig. 1—Stereographic plot of habit-plane normals p. Navruz point is confined to the (0 k l) line 7.3 deg from observation. The WLR/BM point is 1.7 deg from observation. The Ledbetter–Dunn point is 1.7 deg from observation, taking a twinning fraction of 0.40. For the WLR/BM case, the twinning fraction is 0.38. If the martensite-plate aspect ratio is increased slightly from zero, the Ledbetter–Dunn theory gives exact agreement with observation.

Using an infinitesimal-deformation approach, Ledbetter and Dunn^[8] found that $\mathbf{p} = (0 \ k \ l)$ if the lattice-invariant deformation is neglected. Later,^[9] they showed that a correct treatment of the lattice-invariant deformation moves the predicted \mathbf{p} from $(0 \ k \ l)$ through the unit triangle up to the $(h \ h \ l)$ line, that line corresponding to equal twin volumes. Thus, we conclude that the Navruz formulation is confined to predict $(0 \ k \ l)$ habit planes near (011) and provides no useful alternative to the WLR/BM invariant-plane-strain approaches nor to the Ledbetter–Dunn infinitesimal-deformation approach, which includes WLR/BM as a special case, the zero-elastic-strain-energy case.^[10] Figure 1 also shows the prediction of the Ledbetter–Dunn theory.

REFERENCES

- 1. N. Navruz: Metall. Mater. Trans. A, 2001, vol. 32A, pp. 247-50.
- M. Watanabe and C. Wayman: Metall, Trans., 1971, vol. 2, pp. 2221-27
- M. Watanabe and C. Wayman: Metall. Trans., 1971, vol. 2, pp. 2229-36.
- M. Wechsler, D. Lieberman, and T. Read; Trans. AIME, 1953, vol. 194, p. 1503.
- J. Bowles and J. Mackenzie: Acta Metall., 1954, vol. 2, pp. 129, 138, 221
- A. Khachaturyan: Theory of Structural Phase Transitions, Wiley, New York, NY, 1983, pp. 380, and 396.
- T. Mura, T. Mori, and M. Kato: J. Mech. Phys. Solids, 1976, vol. 24, p. 305
- H. Ledbetter and M. Dunn: in Displacive Phase Transformations and their Applications in Materials Engineering, TMS, Wattendale, 1998, pp. 341-47.
- H. Ledbetter and M. Dunn; Mater. Sci. Eng. A, 1999, vols. A273
 –A275, pp. 222-25.
- H. Ledbetter and M. Dunn: Mater. Sci. Eng. A, 2000, vol. A285, pp. 180-5.

^{*}N. NAVRUZ: Metall. Mater. Trans. A, 2001, vol. 32A, pp. 247-50, HASSEL LEDBETTER, Research Metallurgist, is with the Materials Science and Engineering Laboratory, NIST, Boulder, CO 80305, MARTIN DUNN, Associate Professor, is with the Mechanical Engineering Department, University of Colorado, Boulder, CO 80309.

Author's Reply

NURTEN NAVRUZ

I do not accept the validity of Ledbetter and Dunn's comments for the following reasons:

When a physical quantity is measured n times (x₁, x₂, ... x_n), the best estimate of the true value (the mean) is given by

$$X_n = \frac{1}{n} \sum_{i=1}^n x_i \tag{1}$$

Any particular measurement, x_i , will differ from the mean value by an error. The accuracy of X_n as an estimate of x_i is the standard error, [1] $\sigma(X_n)$:

$$\sigma(X_n) = \frac{1}{\sqrt{n}} \left[\sum_{i=1}^n \delta_i^2 \right]^{1/2}$$
 [2]

where δ_i , the deviation of each measurement is

$$\delta_i = x_i - X_a \tag{3}$$

Thus, the results of an experiment are given in the form

$$X = X_n \pm \sigma(X_n) \tag{4}$$

Using Watanabe and Wayman's 11 measurements for magnitude of the shape deformation listed in Table II, [2] the mean value from Eq. [1] and the standard error from Eq. [2] are obtained:

$$m_1 = 0.1220 \pm 0.0072$$
 [5]

Thus, the error in their measurements is 5.9 pct, unlike

the 20.8 pct claimed by Ledbetter and Dunn. As can be clearly seen, Ledbetter and Dunn's expression, $m_1 = 0.1220 \pm 0.0253$, is incorrect. As a result, since experimental bounds include only Navruz predictions, [3] Navruz predictions and comments on m_1 are valid.

(2) The habit planes given by Navruz are the undistorted planes. As known, in WLR theory, [4] the undistorted habit plane is given in the form $\frac{1}{\sqrt{1+K^2}}$ (0 1 K). In order to make meaningful comparisons with theoretical predictions and observations, the habit plane must be unrotated as well as undistorted. The undistorted plane (**p**) and the invariant plane (**p**') are related by the matrix Γ : therefore.

$$\mathbf{p}' = \Gamma \mathbf{p}$$
 [6]

where

$$\Gamma = \begin{pmatrix} 0.980191 & 0.198060 & 0\\ 0.198056 & 0.980190 & 0\\ 0 & 0 & 1 \end{pmatrix}$$
 [7]

for the fcc \rightarrow bct martensitic transformation with the (110) $1\overline{1}101$ slip system in the Fe-7 pct Al-2 pct C alloy.

Therefore, their comments on the habit plane are not valid.

REFERENCES

- N.C. Barford: Experimental Measurements: Precision, Error and Truth, Addison-Wesley, London, 1967, pp. 25, and 53.
- M. Watanabe and C. Wayman: Metall. Trans., 1971, vol. 2, pp. 2229-36.
- 3. N. Navruz; Metall. Mater. Trans. A, 2001, vol. 32A, pp. 247-50.
- M. Wechsler, D. Lieberman, and T. Read: Trans. AIME, 1953, vol. 194, pp. 1503-15.